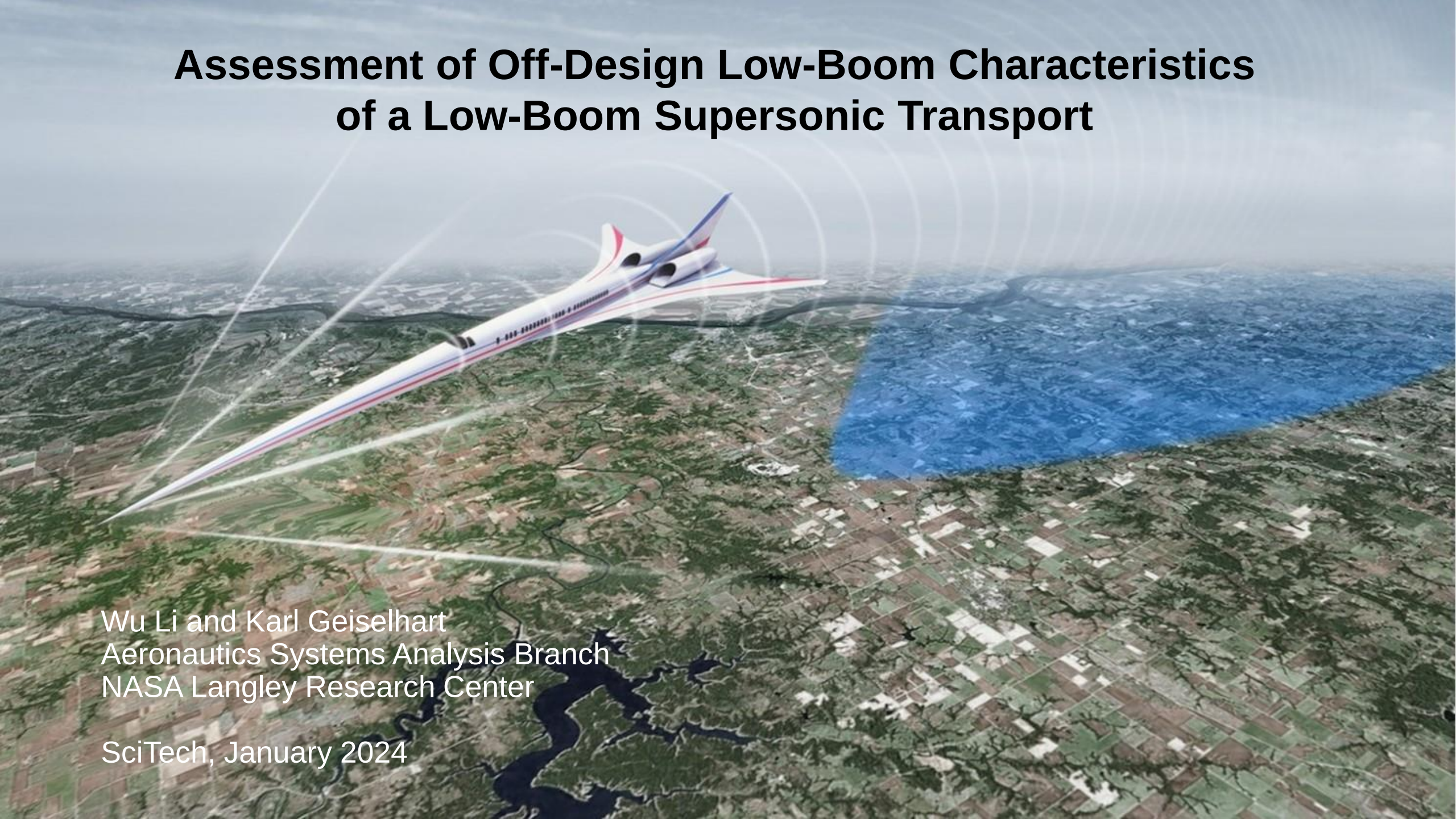


# Assessment of Off-Design Low-Boom Characteristics of a Low-Boom Supersonic Transport



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SciTech, January 2024



- Motivation
- Minimum Requirements for Low-Boom Concepts
- Optimal Mission Profile for Low-Boom Supersonic Aircraft
- Assessment Method for Off-Design Low-Boom Characteristics
- Undertrack Low-Boom Characteristics of Low-Boom Concept
- Off-track Low-Boom Characteristics of Low-Boom Concept
- Conclusions



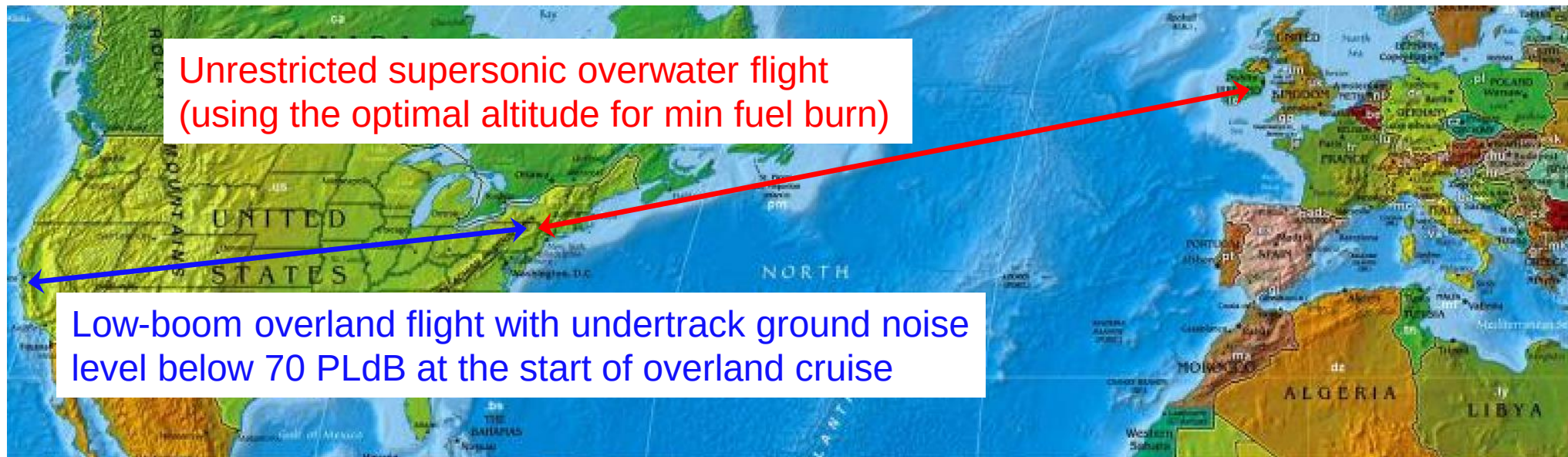
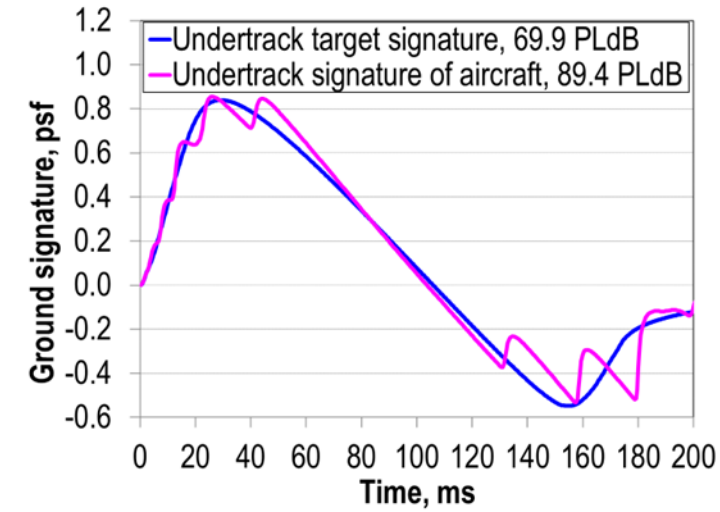
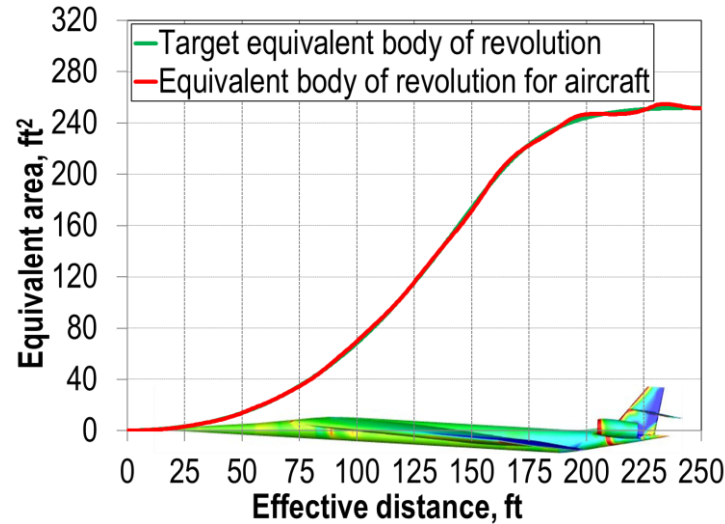
- Multiple studies indicate that the ban on overland supersonic flights has a detrimental impact on the economic viability of supersonic transports.
- NASA has been developing low-boom technologies to enable commercial supersonic overland flights, which will be demonstrated by the X-59.
- Two supersonic transport concepts with 40 passengers were successfully developed to satisfy a conceptual-level low-boom constraint and achieve the required mission performance goals. (Published in [2021](#) and [2022](#))
- How could we generate a supersonic transport concept that has the potential to have the desired low-boom characteristics over the primary boom carpet for the entire cruise segment?



# Minimum Requirements for Low-Boom Supersonic Transports

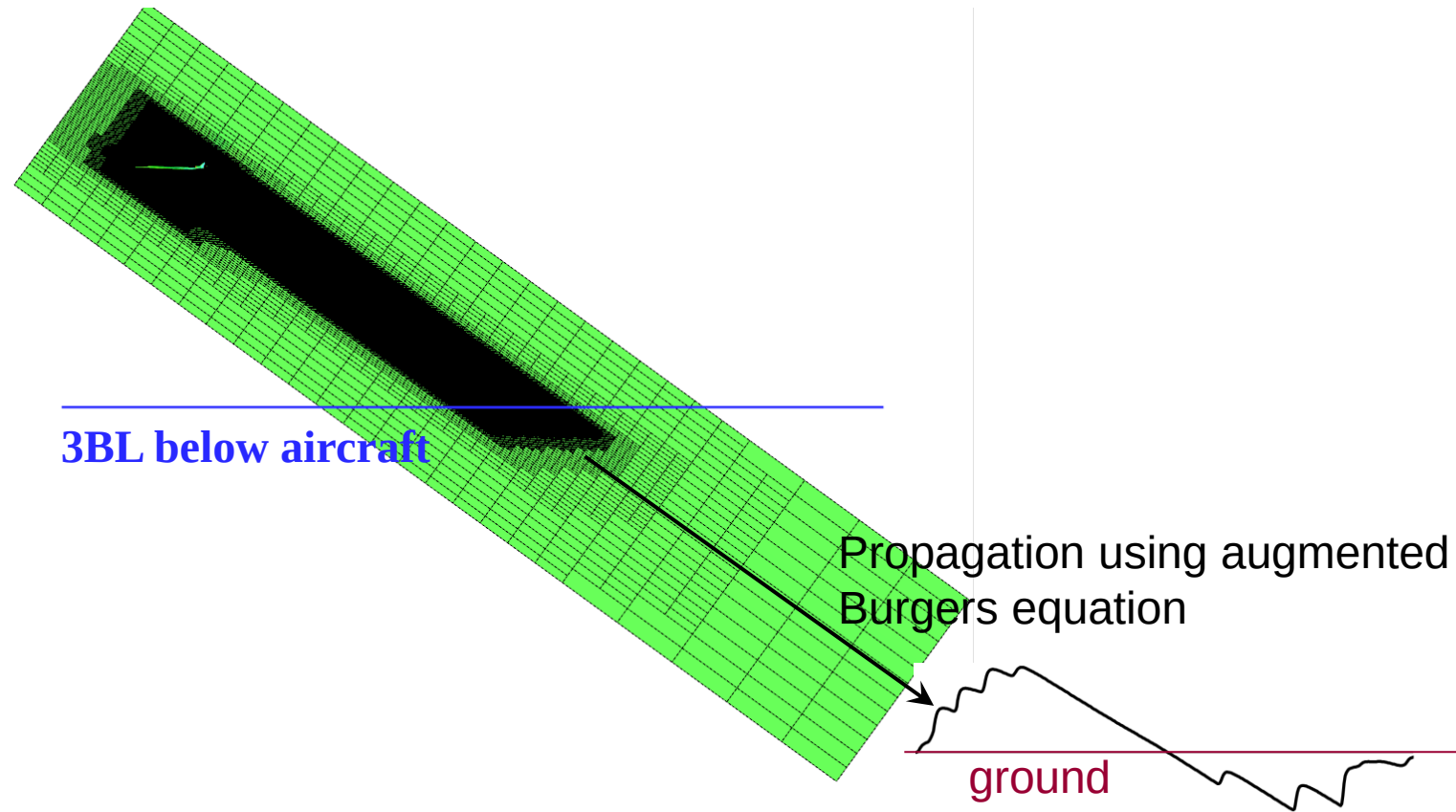
- Overwater range  $\geq 3600$  nm for transatlantic flights, cruise Mach 1.8
- Overland range  $\geq 2500$  nm for airport pairs in continental US
- Overland supersonic flight with cruise Mach  $\geq 1.4$  and sonic boom ground noise level below 70 PLdB (NASA N+3 goal)

## Low-boom constraint at start of overland cruise



# Sonic Boom Analysis Using CFD Off-Body Pressure

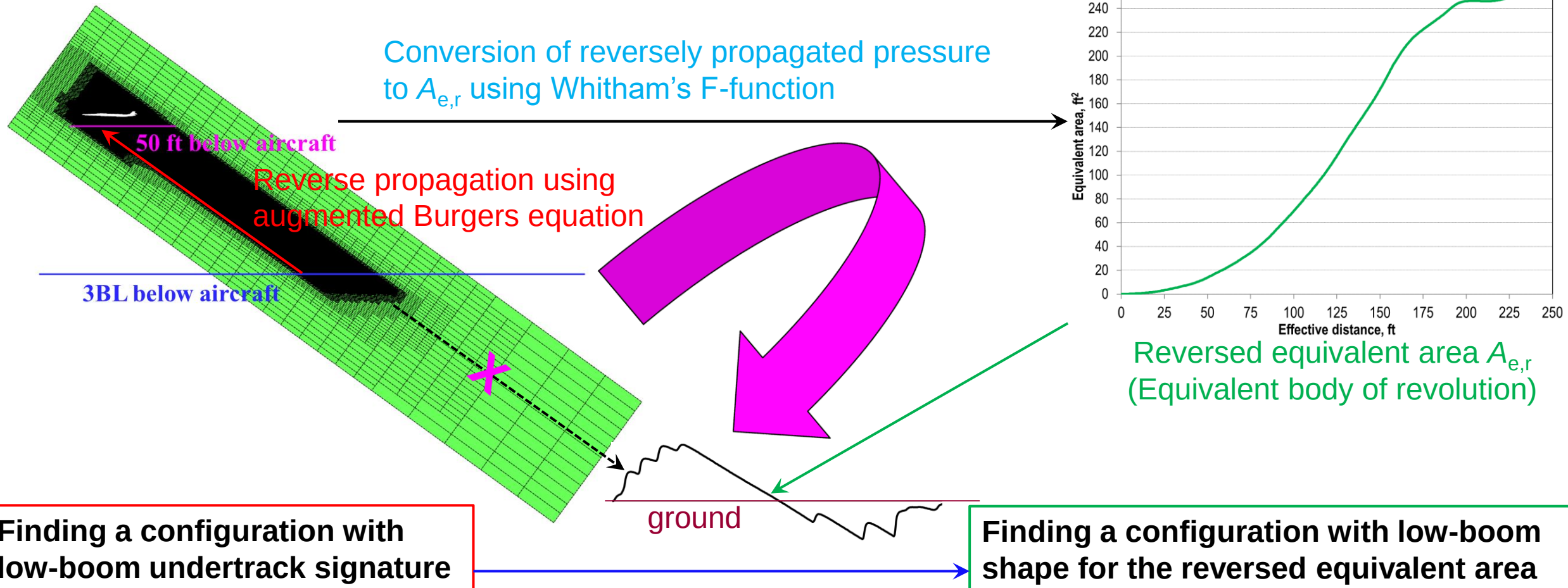
1. Use CFD off-body pressure at the location of 3 body lengths (3BL) below the aircraft.
2. Use an augmented Burgers equation to propagate the CFD off-body pressure through the atmosphere to the ground.
3. Compute the perceived level of decibels (PLdB) of the ground signature.





# Sonic Boom Analysis Using Reversed Equivalent Area

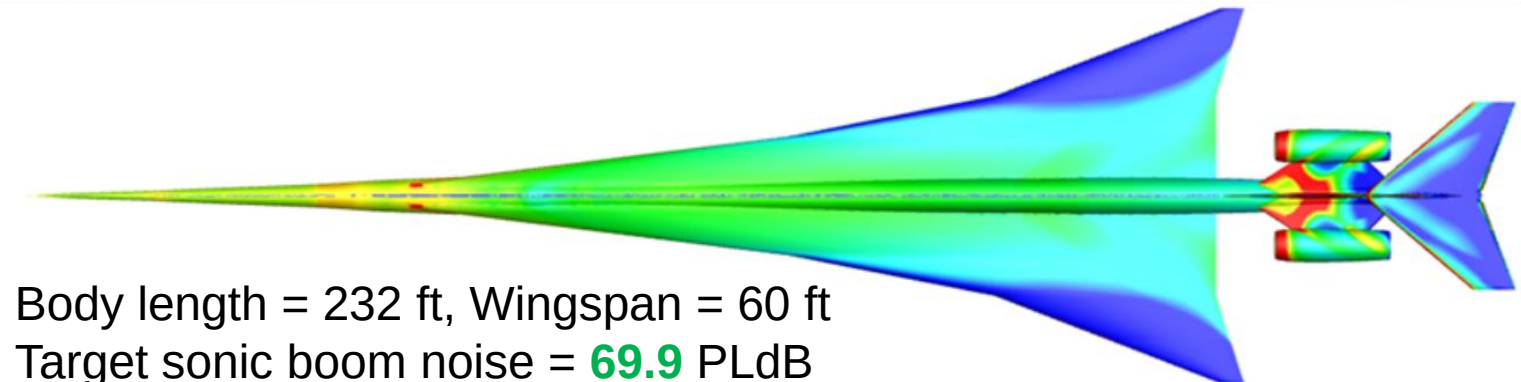
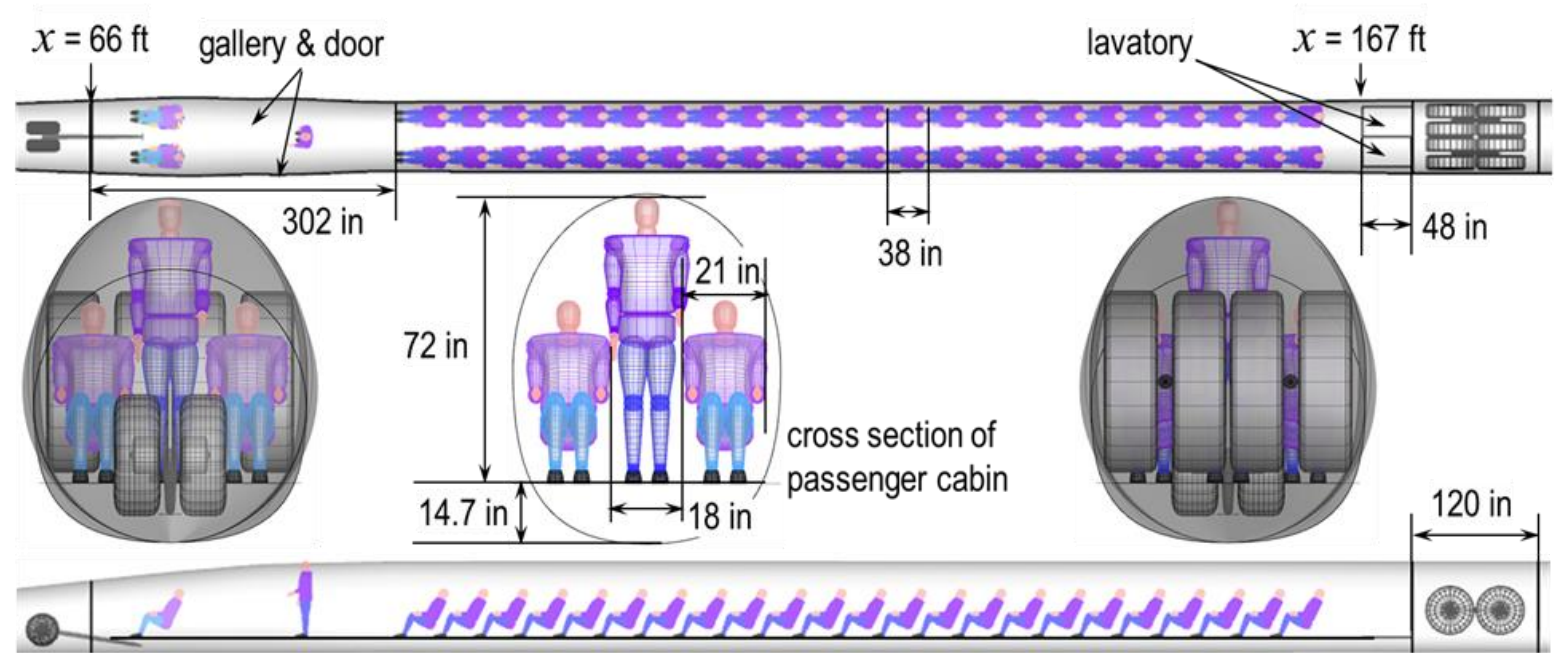
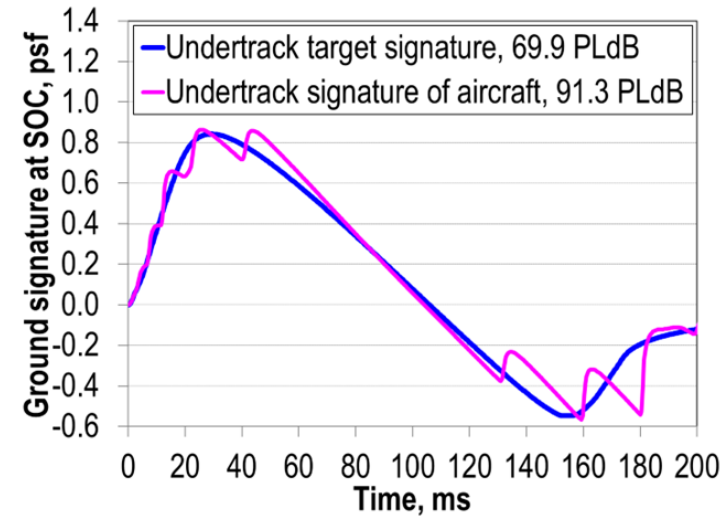
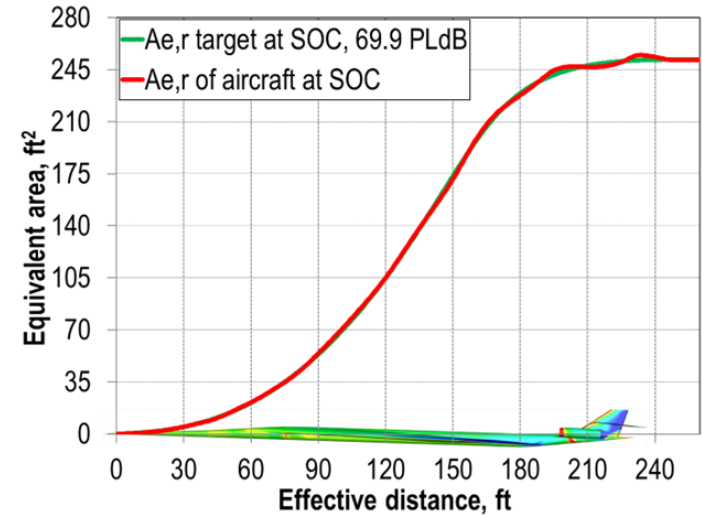
1. Reversely propagate the off-body pressure to 50 ft below the aircraft.
2. Convert the reversely propagated pressure to equivalent area.
3. Propagate the equivalent area to the ground and compute its PLdB value.





# Low-Boom Concept at Start of Overland Cruise (SOC)

| Concept | Passenger No. | MTOGW      | OL Mach | OL Range | OW Mach | OW Range |
|---------|---------------|------------|---------|----------|---------|----------|
| 46-PAX  | 46            | 147,600 lb | 1.7     | 3317 nm  | 1.8     | 3671 nm  |



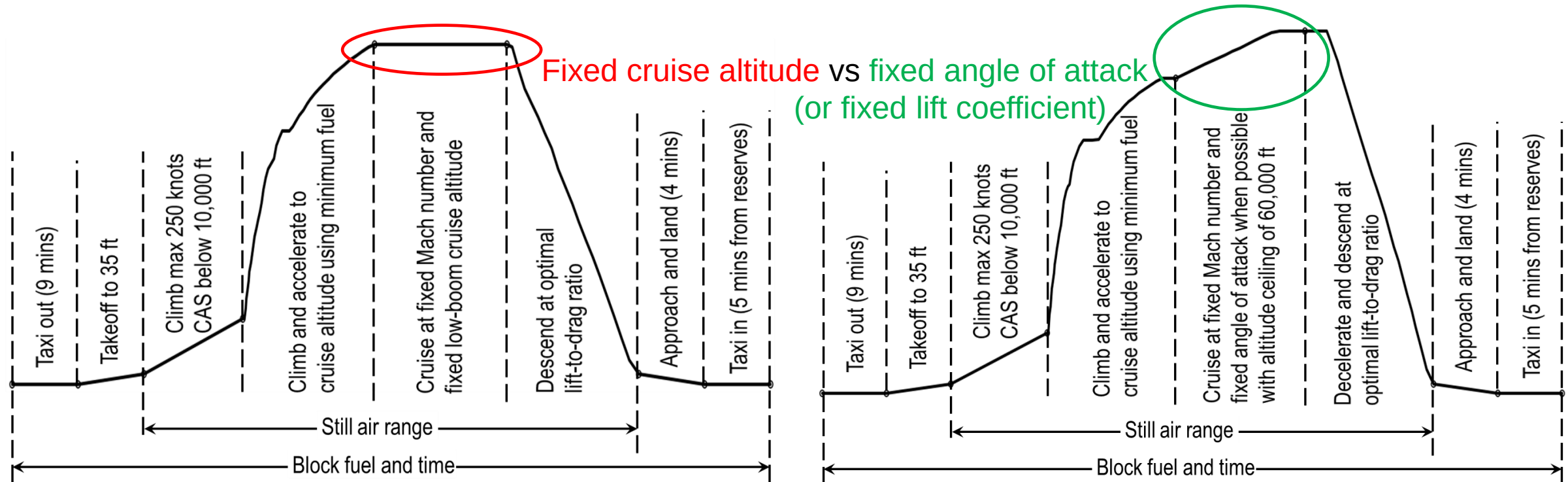
Body length = 232 ft, Wingspan = 60 ft  
 Target sonic boom noise = **69.9** PLdB

# Optimal Mission Profile for Low-Boom Supersonic Concept



Two advantages of the low-boom mission profile with fixed angle of attack for cruise:

- Easier to retain the designed low-boom characteristics at the start of cruise.
- Better fuel efficiency for cruise.

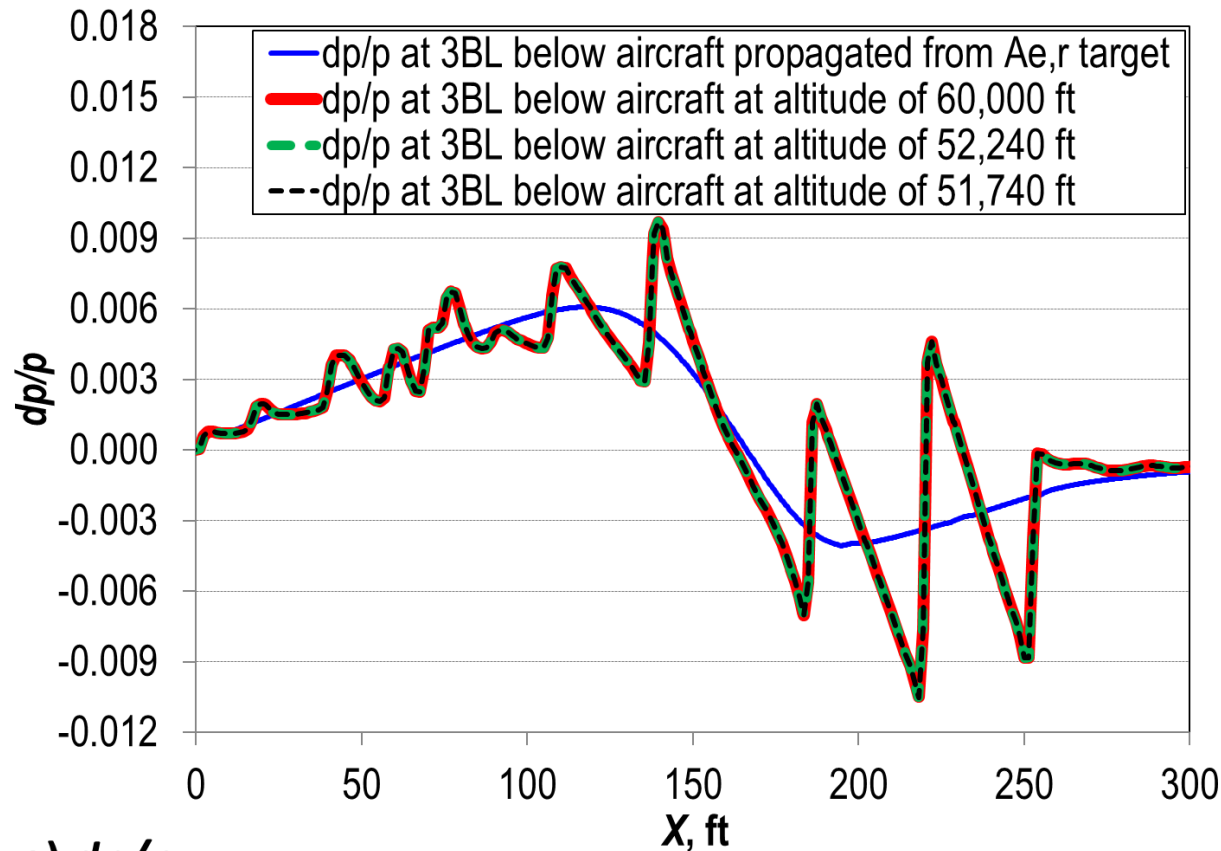




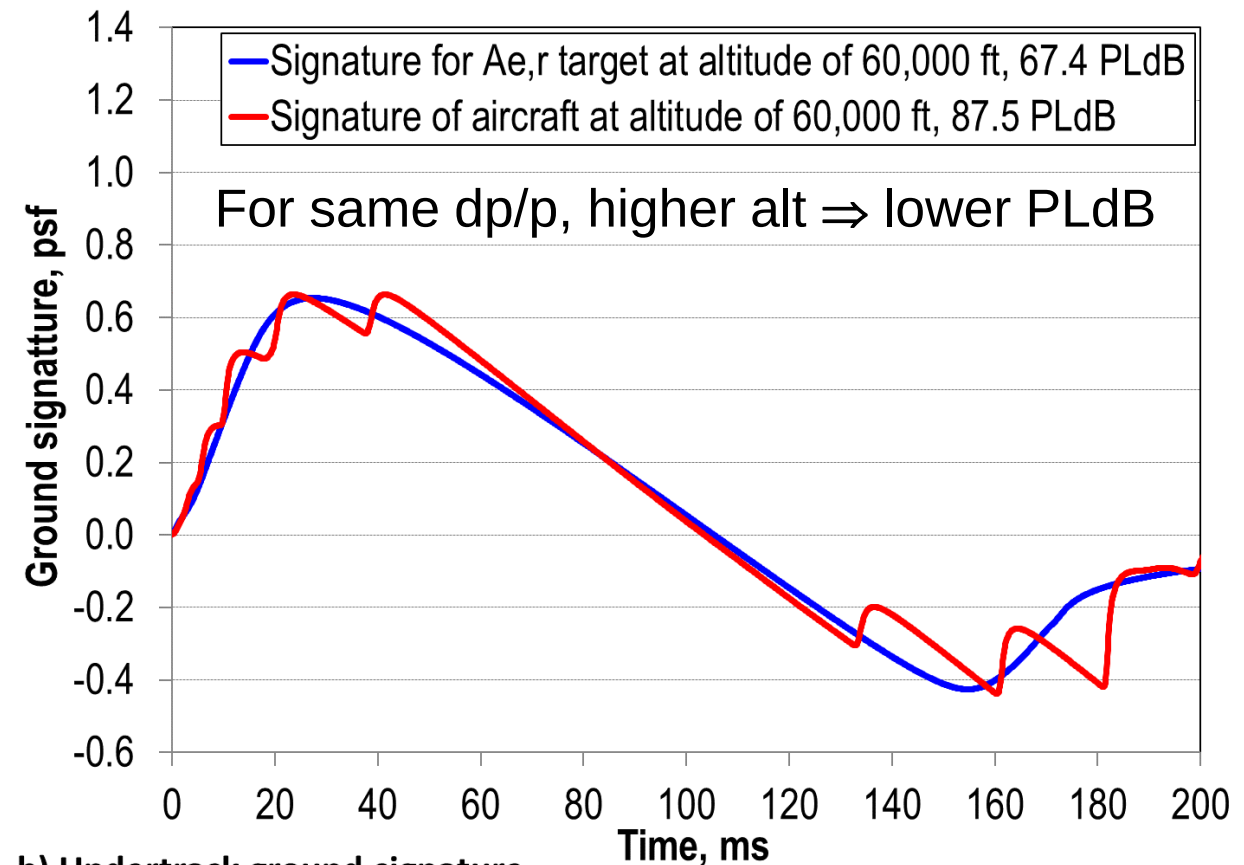
# Benefits of Optimal Mission Profile for Low-Boom Concept



| OL Cruise Constraint | Passenger No. | MTOGW      | OL Mach | OL Range | OW Mach | OW Range |
|----------------------|---------------|------------|---------|----------|---------|----------|
| Fixed Altitude       | 46            | 147,600 lb | 1.7     | 3317 nm  | 1.8     | 3671 nm  |
| Fixed AoA            | 46            | 147,600 lb | 1.7     | 3725 nm  | 1.8     | 3671 nm  |



a)  $dp/p$



b) Undertrack ground signature



# Assessment of Off-Design Low-Boom Characteristics

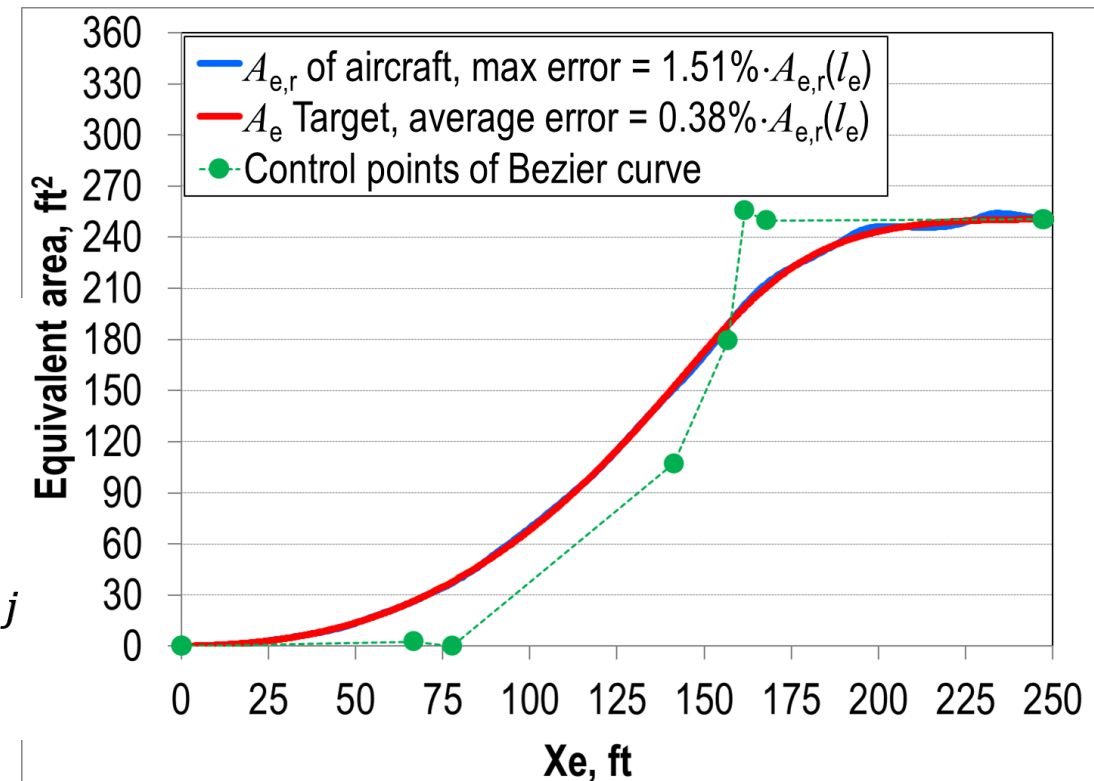
Find an equivalent area target with the lowest PLdB value while having an acceptable inverse design error.

$$\min_{\mathbf{d}} \text{PLdB}[A_e(\theta)] \text{ subject to } \begin{cases} \|A_e(\theta) - A_{e,r}(\theta)\| \leq \epsilon & \text{(acceptable inverse design)} \\ A_e(0) = A'_e(0) = A'_e(l_e) = 0 & \text{(Whitham's theory)} \end{cases}$$

The design vector  $\mathbf{d}$  consists of coordinates of control points of a Bezier curve as a parametric form of  $A_e$ .

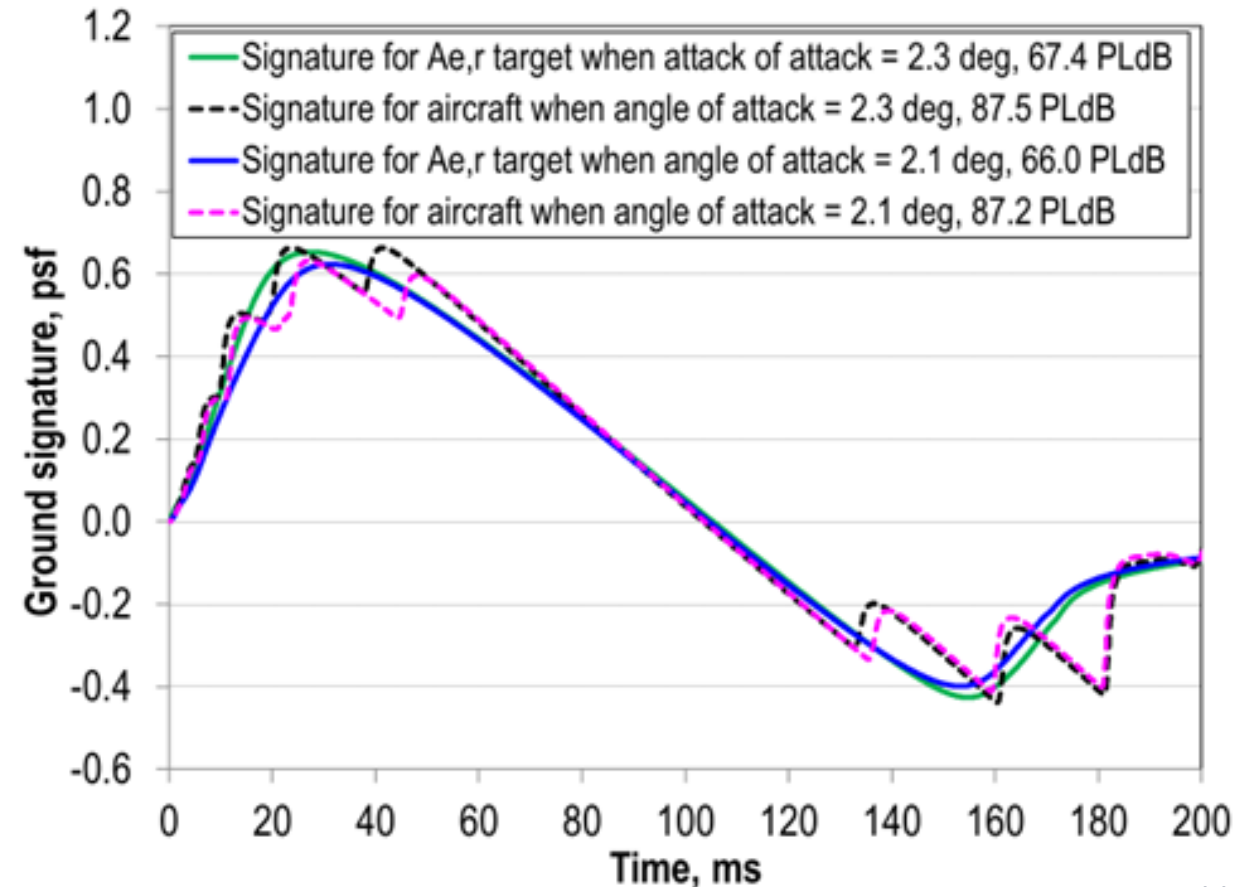
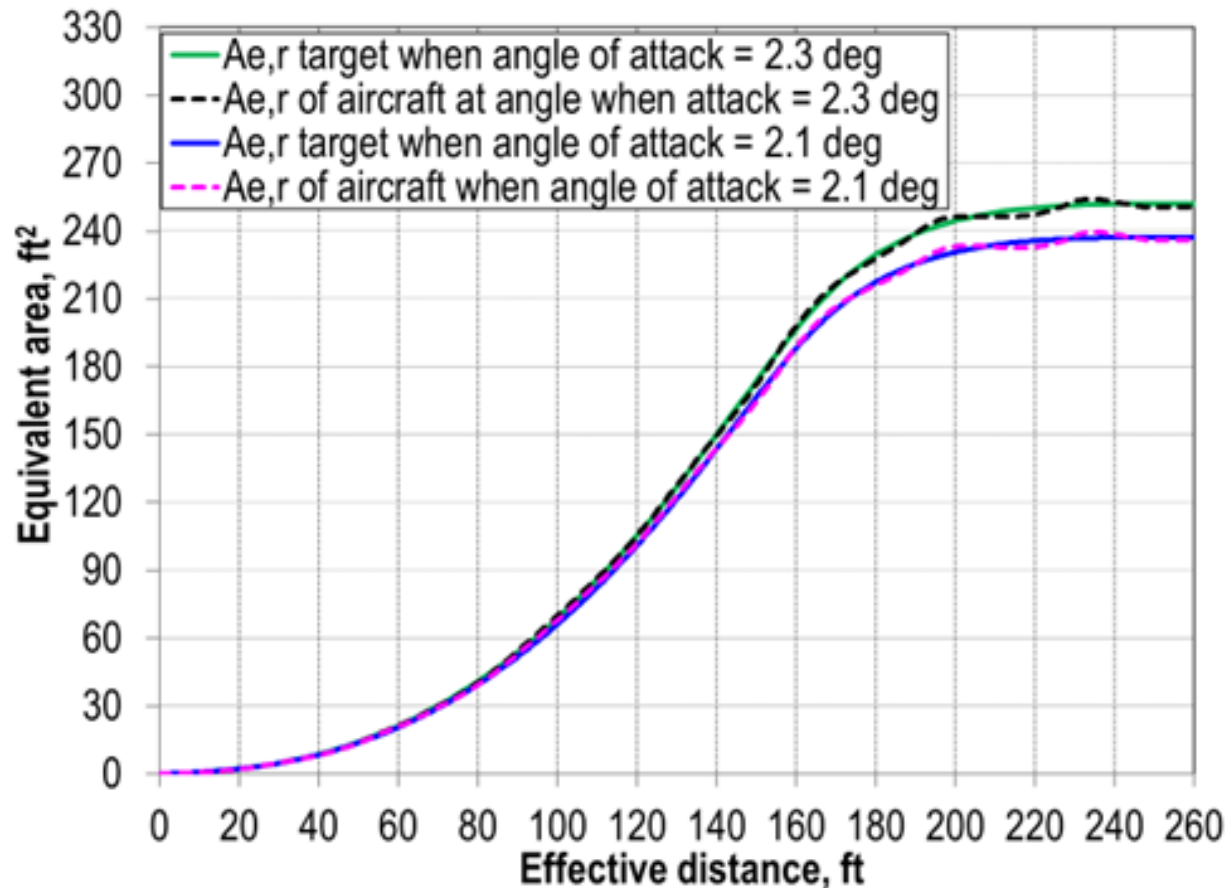
$$x(t) = l_e \cdot t^9 + \sum_{j=1}^8 x_{c,j} \cdot \frac{9!}{j! (9-j)!} \cdot t^j \cdot (1-t)^{9-j}$$

$$A_e(x(t)) = y_{c,8} \cdot t^9 + \sum_{j=2}^8 y_{c,j} \cdot \frac{9!}{j! (9-j)!} \cdot t^j \cdot (1-t)^{9-j}$$



# Undertrack Low-Boom Characteristics for Cruise Segment

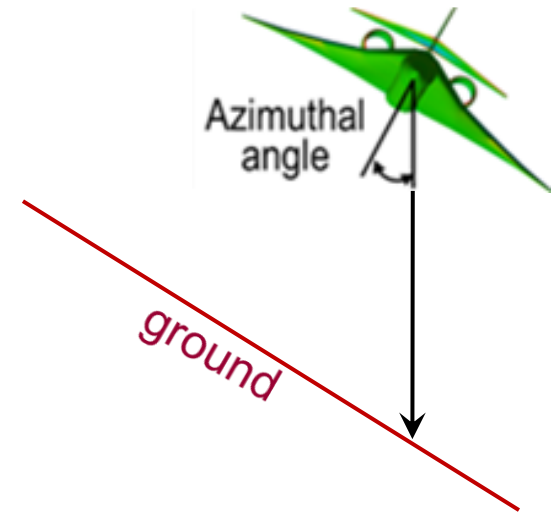
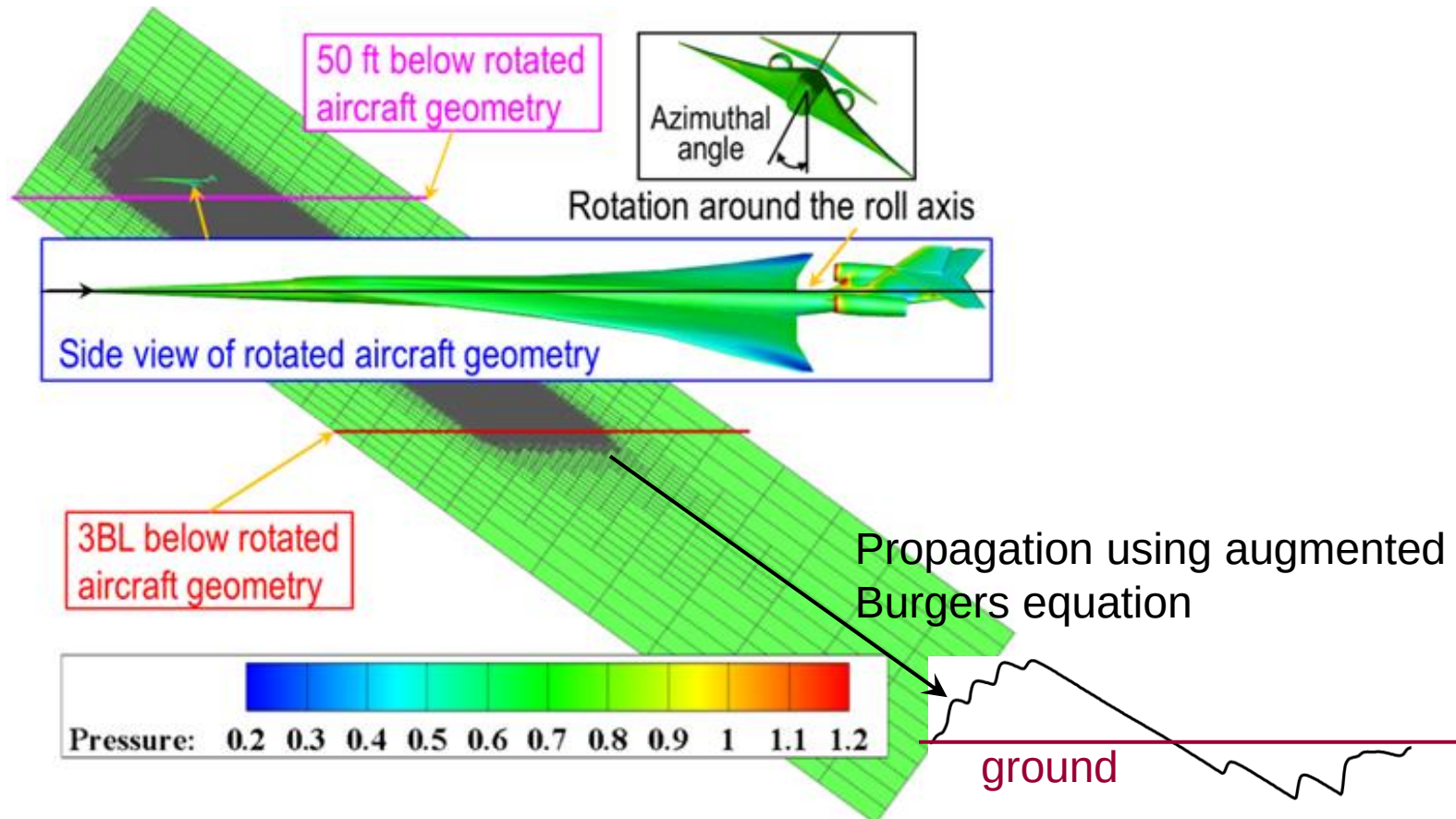
For the 46-PAX concept, the low-boom characteristics at the end of low-boom cruise are better than those at SOC. This is due to the reduced cruise weight and increased cruise altitude.





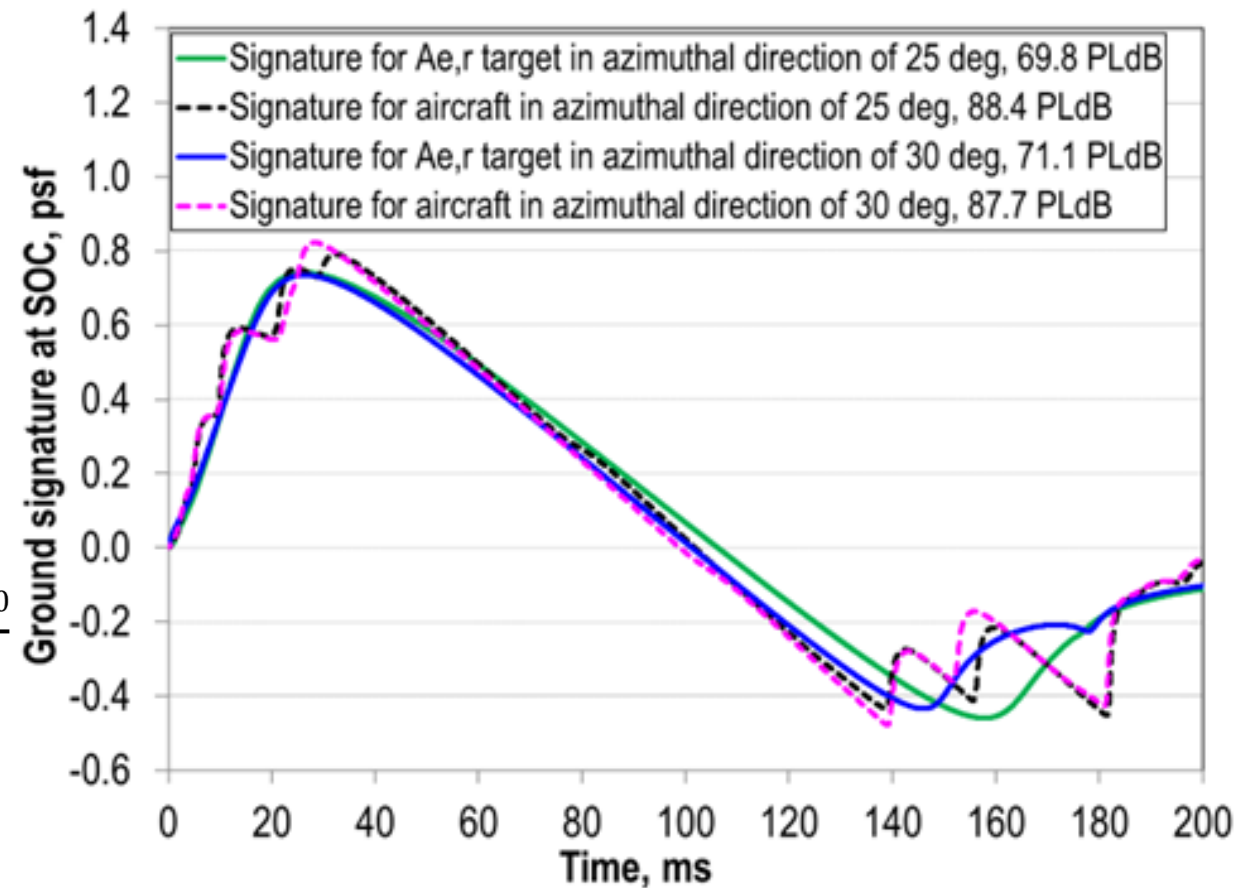
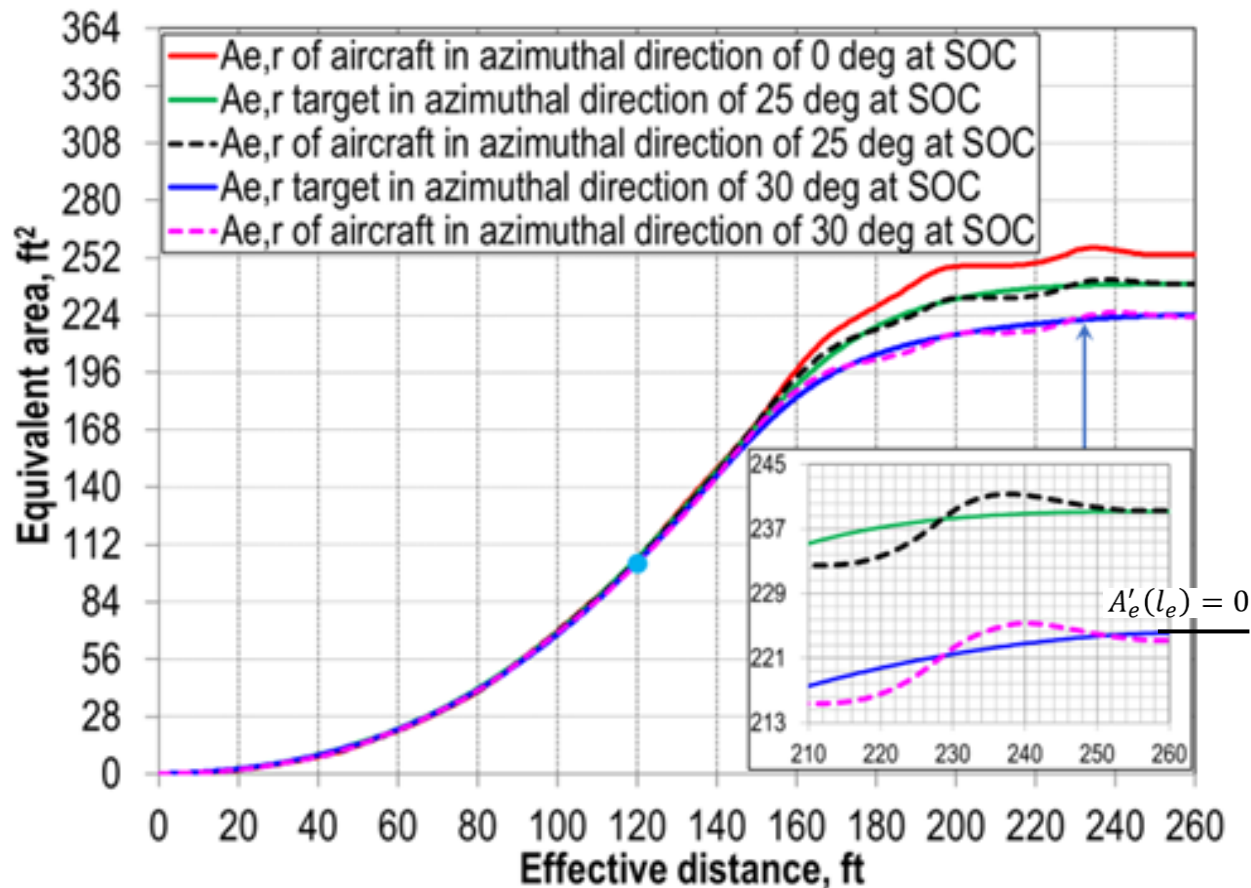
# Off-Track Sonic Boom Analysis

1. Use CFD off-body pressure at the location of 3BL below the **rotated** aircraft.
2. Use an augmented Burgers equation to propagate the CFD off-body pressure along the azimuthal direction through the atmosphere to the ground.
3. Compute the perceived level of decibels (PLdB) of the ground signature.



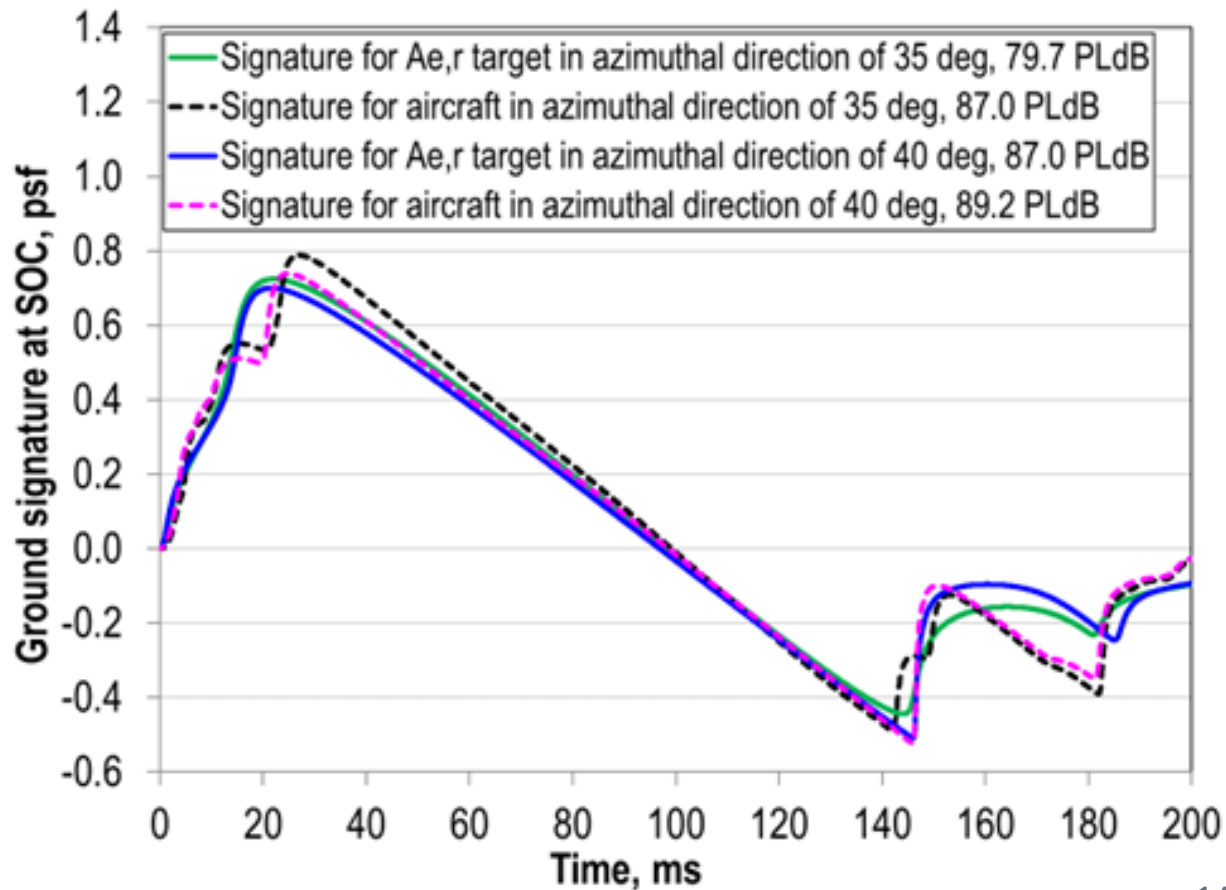
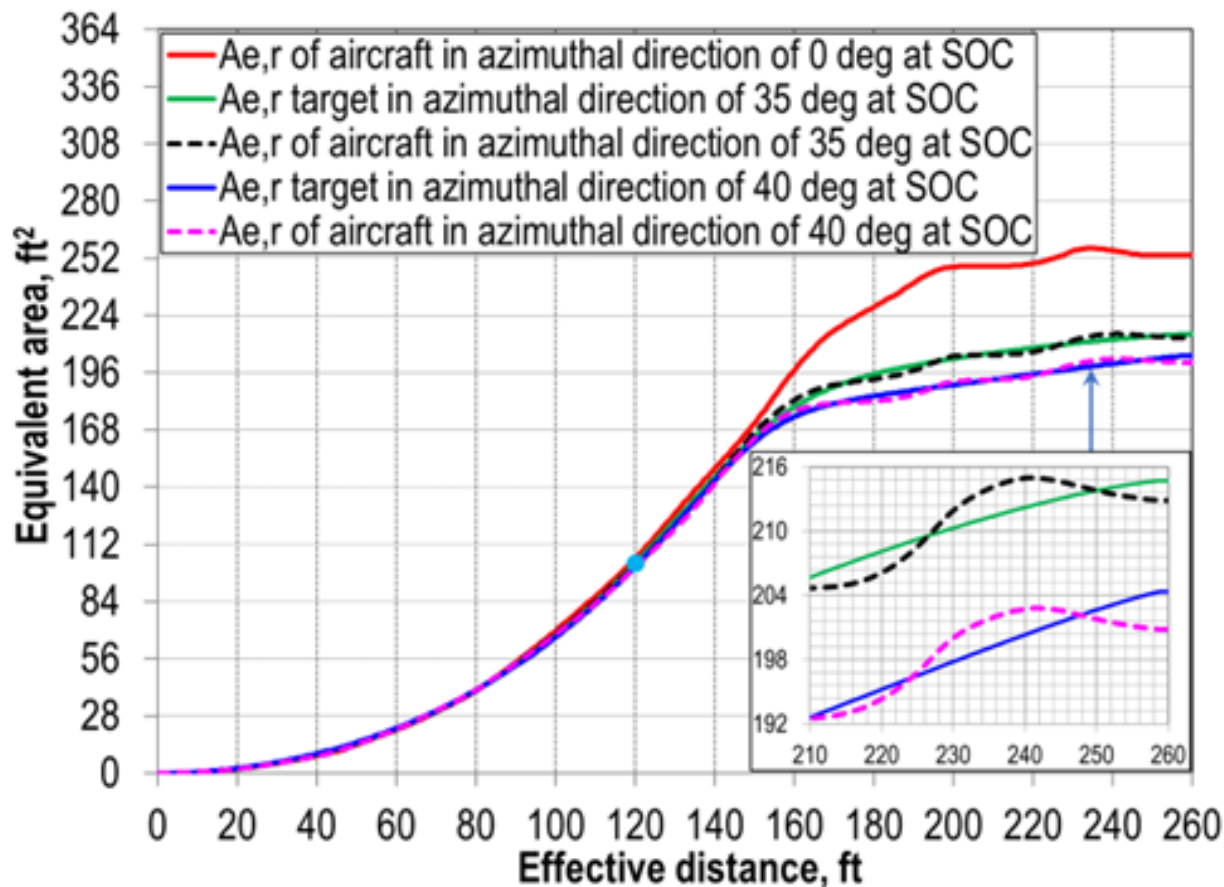
# Off-Track Low-Boom Characteristics at Start of Cruise (I)

- The 46-PAX concept behaves like a body of revolution for effective distance < 120 ft.
- The aft low-boom characteristics starts to deteriorate for off-track angle = 30 deg.

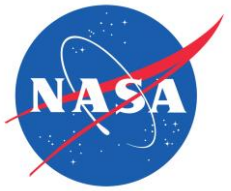


# Off-Track Low-Boom Characteristics at Start of Cruise (II)

- The 46-PAX concept behaves like a body of revolution for effective distance  $< 120$  ft.
- The aft shape of the equivalent area target has an almost linear area increase for off-track angle  $\geq 35$  deg.



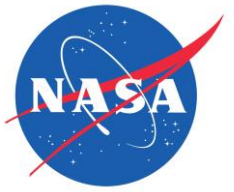




- This work suggests that within the low-boom design space, there exist configurations capable of retaining favorable low-boom characteristics throughout cruise, while maintaining a constant-CL cruise state that maximizes range.
- The analysis method for assessment of off-design low-boom characteristics can be used to screen out supersonic configurations not feasible for robust low-boom design over the primary boom carpet for the entire cruise segment.

# Acknowledgement

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This work is funded by the NASA Commercial Supersonic Technology (CST) Project.

